

**ADDENDUM #1  
LIFT STATION NO. 14 RECONSTRUCTION  
CITY OF DULUTH  
PROJECT NO. 0858SN  
BID NO. 13-0073  
FEBRUARY 8, 2013**

**NOTICE**

Page 1 of 2

This Addendum is issued to modify, explain or correct the original drawings, specifications and/or previous addendums and is hereby made a part of the Contract Documents. Please attach this Addendum to the specifications in your possession and note receipt of this Addendum on The Request For Bid. The bid date remains unchanged.

**PROJECT SPECIFICATIONS**

SPECIAL PROVISIONS

**Table of Contents**

**Delete** “SP-4 (1903) Increased or Decreased Quantities” from the Special Provision Table of Contents.

**ADD** “SP-4 Geotechnical Report” to the Special Provision Table of Contents.

**ADD** the following Special Provisions:

“**SP-4.0** The information contained in the geotechnical report is for borings conducted near Sta. 11+00 to Sta. 11+50 as part of the Goodwill Building Addition referenced on the drawings.”

**ADD** the following Attachment to the Contract Documents:

“Geotechnical Report titled “Geotechnical Investigation And Report, Goodwill Industries – Loading Dock Addition”, dated November 30, 2011..

DIVISION 44

**REPLACE** Section 44 42 56.40, Page3, Part 2.01, Paragraph B with the following paragraph:

- B. Submersible pumps shall be manufactured by KSB (represented by Quality Flow Systems, New Prague, MN) Model KRT F 100-185; Flygt (represented by Electric Pump, New Prague, MN) Model DP 3102 MT 3-471, or approved equal. Written requests for approval of alternate pumps including catalog cuts, certified pump curves, and documentation of conformance or deviation from this specification must be received no later than 10 working days prior to the bid opening.

END OF ADDENDUM



November 30, 2011

Project No. 113-81079

Ms. Marge Bray  
Goodwill Industries  
700 Garfield Avenue  
Duluth, MN 55802

**RE: GEOTECHNICAL INVESTIGATION AND REPORT  
GOODWILL INDUSTRIES- LOADING DOCK ADDITION  
DULUTH, MINNESOTA**

Dear Ms Bray:

Golder Associates, Inc. (Golder) is pleased to submit this report to provide recommendations for the planned renovations at Goodwill Industries.

## **1.0 PROJECT INFORMATION**

The project consists of improvements to the Goodwill Industries Building on Garfield Avenue in Duluth, Minnesota. Improvements include adding an escalator/elevator and a 12 foot by 24 foot loading dock off the north side of the warehouse. We understand the existing building has frost –depth spread footings, and if soil conditions are similar, KOA would like to design a concrete foundation wall extending from a minimum of frost depth (or matching existing footing depth) to 4 ft above exterior grade. Then a pre-engineered metal building will be placed on top.

## **2.0 FIELD INVESTIGATION RESULTS**

The subsurface exploration consisted of drilling and sampling one borehole within the proposed development is shown in Figure 1. The boring was advanced to a depth of 25 ft below existing grade, and encountered five feet of loose fill overlying the native soil. The fill consists of sand with silt and gravel. The native soil consists of poorly graded sand with gravel, and was loose to seven feet below grade, medium dense to 14 feet below grade, and dense below 14 feet.

The borehole was drilled by EPC Engineering and Testing, under the direction of a Golder Senior Engineering Technician. Samples of the soil were obtained by driving a 2-inch outside diameter (O.D.) split spoon sampler ahead of the 4.25" Hollow-Stem Auger. Split spoon samples were collected at 2-ft intervals to a depth of 15 feet below grade, then sampled at 5-foot intervals to a depth of 25 feet. The sampler was driven using a 140-lb automatic drop hammer free falling 30 inches. The number of blows required to drive the sampler each 6-inch interval of the sampling attempt is recorded on the borehole log. In addition, the total number of blows required to advance the sampler through the 6-in. to 18-in. sampling interval is presented as "N" on the borehole log. The blow counts shown on the borehole log are field values that have not been corrected for overburden, sampler size or other factors.

Following completion of borings, the borehole was backfilled with auger cuttings. The boring log was generated by a Golder Engineer who reviewed the driller's field logs and recovered samples. Soils encountered were visually classified according to the United Soils Classification System (USCS) that is summarized in Figure 2. The borehole log is presented as Figure 3.

\\dul1-s-fs1-vm\projects\projects\2011\113-81079 koa goodwill\final reports\113-81079 goodwill report final 11-30-11.docx

Golder Associates Inc.  
4438 Haines Road  
Duluth, MN 55811 USA

Tel: (218) 724-0088 Fax: (218) 724-0089 www.golder.com



Golder Associates: Operations In Africa, Asia, Australasia, Europe, North America and South America

### 3.0 LABORATORY TEST RESULTS

Laboratory tests were performed by Golder Associates Inc. to measure selected Index properties of the samples. Moisture content tests were conducted on all samples according to procedures described in ASTM D2216. Grain Size Distribution Tests were performed on two samples in accordance with ASTM procedures C136 and C117. The results of the laboratory testing are summarized below and are shown graphically as Figure 4.

**TABLE 1**  
**Summary of Laboratory Testing**

Boring Number	Sample Depth (below grade)	Moisture Content (%)	Gravel (%)	Sand (%)	Passing #200 Sieve (%)
G11-01	.5' – 1.5'	8.1	-	-	-
G11-01	2.0' – 4.0"	11.9	4.5	90.7	5.8
G11-01	4.0' – 5.0'	14.0	-	-	-
G11-01	5.0' – 6.0'	11.7	-	-	-
G11-01	7.0' – 8.5'	22.6	-	-	-
G11-01	9.5' – 11.0'	22.6	0.0	98.6	1.4
G11-01	12.0' – 13.5'	21.3	-	-	-
G11-01	14.5' – 16.0'	19.1	-	-	-
G11-01	19.5' – 21.0'	27.6	-	-	-
G11-01	24.5' – 26.0'	26.2	-	-	-

### 4.0 RECOMENDATIONS

We recommend the foundations be provided with a minimum of 72 inches of soil cover for protection from possible frost action. Thus for a one foot thick footing, the bottom of footing would be at seven feet below grade. We understand this is similar or lower than footings for the existing building, so the new addition footings would not transfer additional load on the existing footings.

Foundations constructed on the undisturbed native soils encountered at a depth of seven feet below grade, or on compacted engineered fill placed directly over the dense undisturbed native soils can be designed for an allowable bearing pressure of 3000 psf. If any soft soils exist in the foundation excavation, or if surface disturbance does occur, any soft soils should be removed and replaced with compacted engineered fill. Golder estimates that total and differential settlements should be less than 1 inch and ½ inch, respectively.

All fill placed within the building footprint, and for backfill of building foundations should be an engineered fill meeting the following gradation specifications.

**Table 2**  
**Recommended Gradation for Engineered Fill**

<b>U.S. Standard Sieve Size</b>	<b>Percent Passing</b>
4"	100
2"	80 – 100
#4	60 – 100
#200	0 – 10

Engineered fill within the building footprint should be placed in thin, loose lifts, and compacted to 95% of modified Proctor dry density as determined by ASTM Test Method D1557.

## **5.0 STANDARD OF CARE**

This report was prepared for the exclusive use of KOA and Goodwill Industries for use during design of the planned loading dock addition to Goodwill. We understand that we may be contacted as the design finalizes and the construction process begins so we can verify the proposed construction conforms to our engineering recommendations.

There are possible variations in subsurface conditions between explorations and also with time. Therefore, inspection and testing by a qualified geotechnical engineer should be included during construction to provide corrective recommendations adapted to the conditions revealed during the work.

Unanticipated soil conditions are commonly encountered that cannot fully be determined by a limited number of explorations and inspections. Such unexpected conditions frequently result in additional project costs in order to build the project as designed. Therefore, a contingency for unanticipated conditions should be included in the construction budget and schedule.

Inspection and testing by a qualified structural/geotechnical engineer should be included during construction to provide corrective recommendations adapted to the conditions revealed during the work.

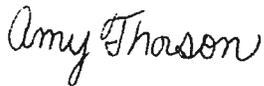
The work program followed the standard of care expected of professionals undertaking similar work in the State of Minnesota under similar conditions. No warranty expressed or implied is made.

## 6.0 CLOSING

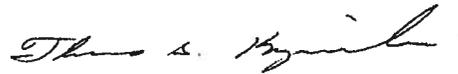
We trust that this report provides you with the information you need to for the design of the planned addition to Goodwill. Please contact Amy Thorson at (218) 724-0088 if you have any questions or if we can assist you further in the design or construction process.

Sincerely,

**GOLDER ASSOCIATES INC.**



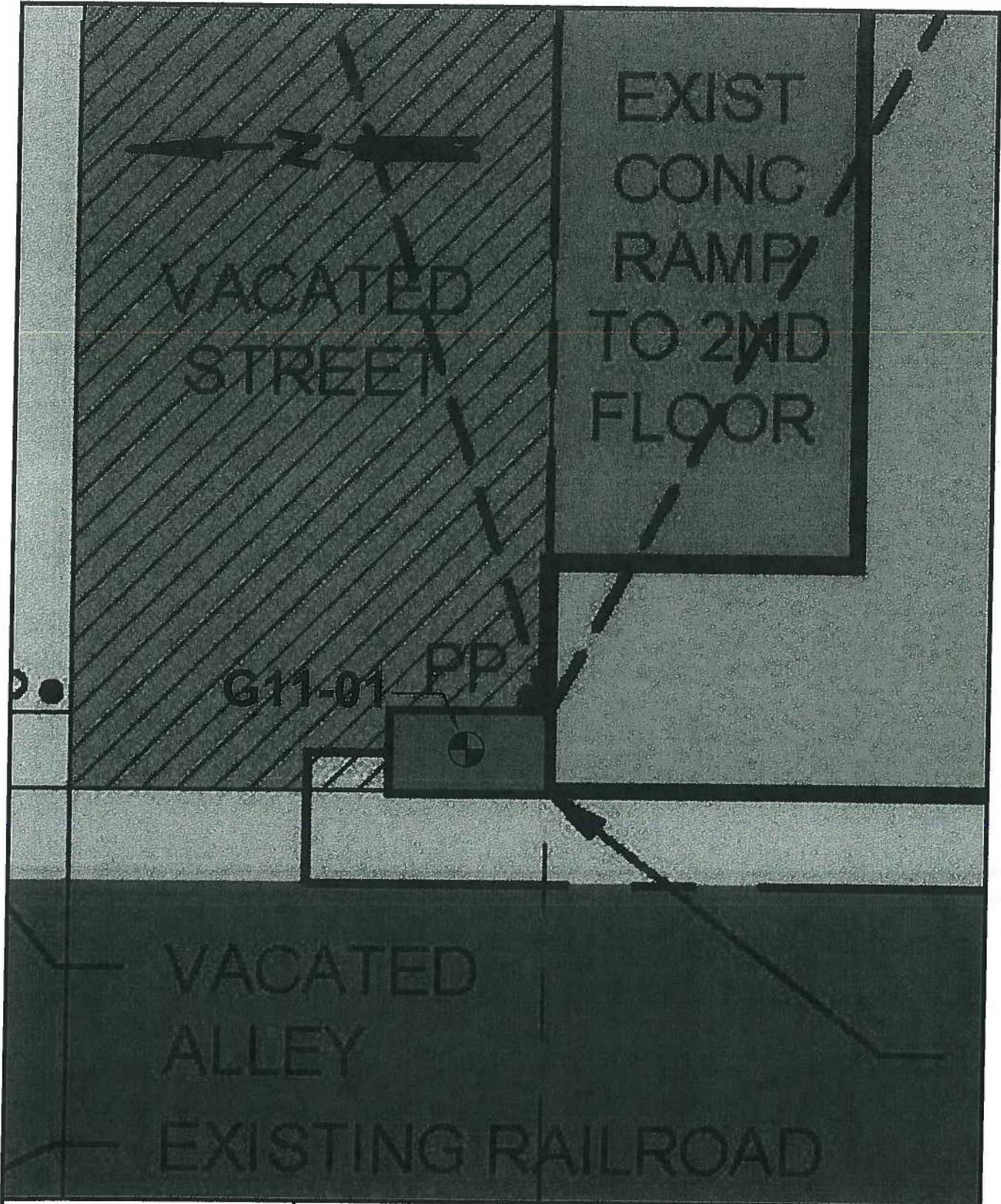
Amy C. Thorson, P.E.  
Senior Engineer, Manager Duluth Operations  
MN License No. 42917



Thomas G. Krzewinski, P.E.  
Principal Geotechnical Engineer  
MN License No. 18391

Figures:        Figure 1 Site Plan  
                  Figure 2 Soil Classification Index/Legend  
                  Figure 3 Record of Borehole G11-01  
                  Figures 4 Grain Size Distribution

CC:     Ms Sara Ojard PE  
         Krech Ojard & Associates  
         227 West First Street, Suite 200  
         Duluth, MN 55802



SCALE 1" = ~20'  
 CADD MTK  
 DATE 11/14/11  
 CHECK ACT

TITLE  
**BOREHOLE LOCATION**  
 GOODWILL INDUSTRIES LOADING DOCK ADDTION  
 DULUTH, MINNESOTA

FILE No. 113-81079\_figure1.DWG  
 PROJECT No. 053-9999x000.0000

DATE 11/14/11  
 REV. 0

GOODWILL / LOADING DOCK / DULUTH, MN

FIGURE 1

## UNIFIED SOIL CLASSIFICATION (ASTM D 2487-00)

MATERIAL TYPES	CRITERIA FOR ASSIGNING SOIL GROUP NAMES AND GROUP SYMBOLS USING LABORATORY TESTS			GROUP SYMBOL	SOIL GROUP NAMES & LEGEND	
COARSE-GRAINED SOILS >50% RETAINED ON NO. 200 SIEVE	GRAVELS >50% OF COARSE FRACTION RETAINED ON NO. 4. SIEVE	CLEAN GRAVELS <5% FINES	$C_u \geq 4$ AND $1 \leq C_c \leq 3$	GW	WELL-GRADED GRAVEL	If soil contains $\geq 15\%$ sand, add "with sand"
			$C_u > 4$ AND/OR $1 > C_c > 3$	GP	POORLY-GRADED GRAVEL	
		GRAVELS WITH FINES >12% FINES	FINES CLASSIFY AS ML OR CL	GM	SILTY GRAVEL	
			FINES CLASSIFY AS CL OR CH	GC	CLAYEY GRAVEL	
	SANDS >50% OF COARSE FRACTION PASSES ON NO. 4. SIEVE	CLEAN SANDS <5% FINES	$C_u \geq 6$ AND $1 \leq C_c \leq 3$	SW	WELL-GRADED SAND	If soil contains $\geq 15\%$ gravel, add "with gravel"
			$C_u > 6$ AND/OR $1 > C_c > 3$	SP	POORLY-GRADED SAND	
SANDS AND FINES >12% FINES		FINES CLASSIFY AS ML OR MH	SM	SILTY SAND		
		FINES CLASSIFY AS CL OR CH	SC	CLAYEY SAND		
FINE-GRAINED SOILS >50% PASSES NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT <50			CL	LEAN CLAY	If soil contains coarse-grained soil from 15% to 29%, add "with sand" or "with gravel" for whichever type is prominent, or for $\geq 30\%$ , add "sandy" or "gravelly"
				ML	SILT	
				OL	ORGANIC CLAY OR SILT	
	SILTS AND CLAYS LIQUID LIMIT $\geq 50$			CH	FAT CLAY	
				MH	ELASTIC SILT	
				OH	ORGANIC CLAY OR SILT	
HIGHLY ORGANIC SOILS	PRIMARILY ORGANIC MATTER, DARK IN COLOR, AND ORGANIC ODOR			PT	PEAT	

Gravels or sands with 5% to 12% fines require dual symbols (GW-GM, GW-GC, GP-GM, GP-GC, SW-SM, SW-SC, SP-SM, SP-SC) and add "with clay" or "with silt" to group name. If fines classify as CL-ML for GM or SM, use dual symbol GC-GM or SC-SM.

$$C_u = \frac{D_{60}}{D_{10}} \quad C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$$

**Optional Abbreviations:** Lower case "s" after USCS group symbol denotes either "sandy" or "with sand" and "g" denotes either "gravelly" or "with gravel"

### RELATIVE DENSITY / CONSISTENCY ESTIMATE USING STANDARD PENETRATION TEST (SPT) VALUES

CRITERIA FOR DESCRIBING MOISTURE CONDITION (ASTM D 2488-00)	
DRY	ABSENCE OF MOISTURE, DUSTY, DRY TO THE TOUCH
MOIST	DAMP BUT NO VISIBLE WATER
WET	VISIBLE FREE WATER, USUALLY SOIL IS BELOW WATER TABLE

COHESIONLESS SOILS <sup>(a)</sup>		COHESIVE SOILS <sup>(b)</sup>		UNCONFINED COMPRESSIVE STRENGTH (TSF) <sup>(d)</sup>
RELATIVE DENSITY	$N_1$ (BLOWS/FOOT) <sup>(c)</sup>	CONSISTENCY	$N_1$ (BLOWS/FOOT) <sup>(c)</sup>	
VERY LOOSE	0 - 4	VERY SOFT	0 - 2	0 - 0.25
LOOSE	4 - 10	SOFT	2 - 4	0.25 - 0.50
COMPACT	10 - 30	FIRM	4 - 8	0.50 - 1.0
DENSE	30 - 50	STIFF	8 - 15	1.0 - 2.0
VERY DENSE	OVER 50	VERY STIFF	15 - 30	2.0 - 4.0
		HARD	OVER 30	OVER 4.0

- (a) Soils consisting of gravel, sand, and silt, either separately or in combination possessing no characteristics of plasticity, and exhibiting drained behavior.
- (b) Soils possessing the characteristics of plasticity, and exhibiting undrained behavior.
- (c) Refer to ASTM D 1586-99 for a definition of  $N_1$ . Values shown are based on  $N_1$  values corrected for overburden pressure ( $N_1$ ).  $N_1$  values may be affected by a number of factors including material size, depth, drilling method, and borehole disturbance.  $N_1$  values are only an approximate guide for frozen soil or cohesive soil.
- (d) Undrained shear strength,  $s_u = 1/2$  unconfined compression strength,  $U_c$ . Note that Torvane measures  $s_u$  and Pocket Penetrometer measures  $U_c$ .

COMPONENT DEFINITIONS BY GRADATION	
COMPONENT	SIZE RANGE
BOULDERS	ABOVE 12 IN.
COBBLES	3 IN. TO 12 IN.
GRAVEL	3 IN. TO NO. 4 (4.76 mm)
COARSE GRAVEL	3 IN. TO NO. 4 (4.76 mm)
FINE GRAVEL	3/4 IN. TO NO. 4 (4.76 mm)
SAND	NO. 4 (4.76 mm) TO NO. 200 (0.074 mm)
COARSE SAND	NO. 4 (4.76 mm) TO NO. 10 (2.0 mm)
MEDIUM SAND	NO. 10 (2.0 mm) TO NO. 40 (0.42 mm)
FINE SAND	NO. 40 (0.42 mm) TO NO. 200 (0.074 mm)
SILT AND CLAY	SMALLER THAN NO. 200 (0.074 mm)
SILT	0.074 mm TO 0.005 mm
CLAY	LESS THAN 0.005 mm

### SAMPLER ABBREVIATIONS

SS SPT Sampler (2 in. OD, 140 lb hammer)	C Core (Rock)
SSO Oversize Split Spoon (2.5 in. OD, 140 lb typ.)	TW Thin Wall (Shelby Tube)
HD Heavy Duty Split Spoon (3 in. OD, 300/340 lb typ.)	MS Modified Shelby
BD Bulk Drive (4 in. OD, 300/340 lb hammer typ.)	GP Geoprobe
CA Continuous Core (Soil in Hollow-Stem Auger)	RC Air Rotary Cuttings
GS Grab Sample from surface / testpit	AG Auger Cuttings

### DESCRIPTIVE TERMINOLOGY FOR PERCENTAGES (ASTM D 2488-00)

DESCRIPTIVE TERMS	RANGE OF PROPORTION
TRACE	0 - 5%
FEW	5 - 10%
LITTLE	10 - 25%
SOME	30 - 45%
MOSTLY	50 - 100%

### LABORATORY TEST ABBREVIATIONS

Con Consolidation	PM Modified Proctor	TXCD Consolidated Drained Triaxial
Dd Dry Density	PP Pocket Penetrometer	TXCU Consolidated Undrained Triaxial
MA Sieve and Hydrometer Analysis	RD Relative Density	TXUU Unconsolidated Undrained Triaxial
NP Non-plastic	SA Sieve Analysis	
OLI Organic Loss	SpG Specific Gravity	
P200 Percent Fines (Silt & Clay)	TS Thaw Consolidation	W <sub>c</sub> Liquid Limit (LL)
PID Photoionization Detector	TV Torvane	W <sub>p</sub> Plastic Limit (PL)

## SOIL CLASSIFICATION / LEGEND

Figure 2



PROJECT: Goodwill Industries - Loading Dock Addition  
 PROJECT NUMBER: 113-81079  
 LOCATION: Loading Dock Addition  
 CLIENT: Krech Ojard & Goodwill Industries

# RECORD OF BOREHOLE G11-01

SHEET 1 of 1

DRILLING METHOD: Hollow-Stem Auger  
 DRILLING DATE: 11-2-11  
 DRILL RIG: 55

DATUM: Ground Surface  
 AZIMUTH: ---  
 COORDS: n/a

GS ELEVATION: ---  
 TOC ELEVATION: ---  
 INCLINATION: -90

DEPTH (ft)	BORING METHOD	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS / ft		NOTES WATER LEVELS GRAPHIC	
		DESCRIPTION	USCS	GRAPHIC LOG	ELEV. DEPTH (ft)	NUMBER	TYPE	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC / ATT	WATER CONTENT (PERCENT)		
											W <sub>p</sub>		W <sub>L</sub>
0.0 - 0.3		Bituminous Pavement - 4" Thickness			0.3								
0.3 - 5.0		Loose, moist, brown, SAND with silt and gravel. (SP-SM, FILL)	SP-SM			1	AUGER			20.0			
						2	SS	2-3-2-2	5	14.0 / 24.0			
						3	SS	3-2	2	9.0 / 12.0			
5.0 - 7.0		Loose, moist, brown, poorly graded SAND with gravel. (SP)	SP		5.0	4	SS	2-2	2	12.0 / 12.0			
7.0 - 14.0		Compact, moist, brown, poorly graded SAND with gravel. (SP)	SP		7.0	5	SS	5-7-10	17	14.0 / 18.0			7 ft 11-2-11 WD
						6	SS	12-12-8	20	14.0 / 18.0			P200 = 1.4%
						7	SS	7-13-13	26	14.0 / 18.0			
14.0 - 26.0		Dense, moist, brown, poorly graded SAND with Gravel. (SP)	SP		14.0	8	SS	12-18-22	40	14.0 / 18.0			
						9	SS	10-17-16	33	15.0 / 18.0			
						10	SS	12-18-17	35	14.0 / 18.0			
		Boring completed at 26.0 ft.											
		<b>NOTES:</b> 1. End of Borehole at 26.0 feet. 2. Groundwater encountered while drilling at 7.0 feet. 3. Borehole backfilled with auger cuttings.											

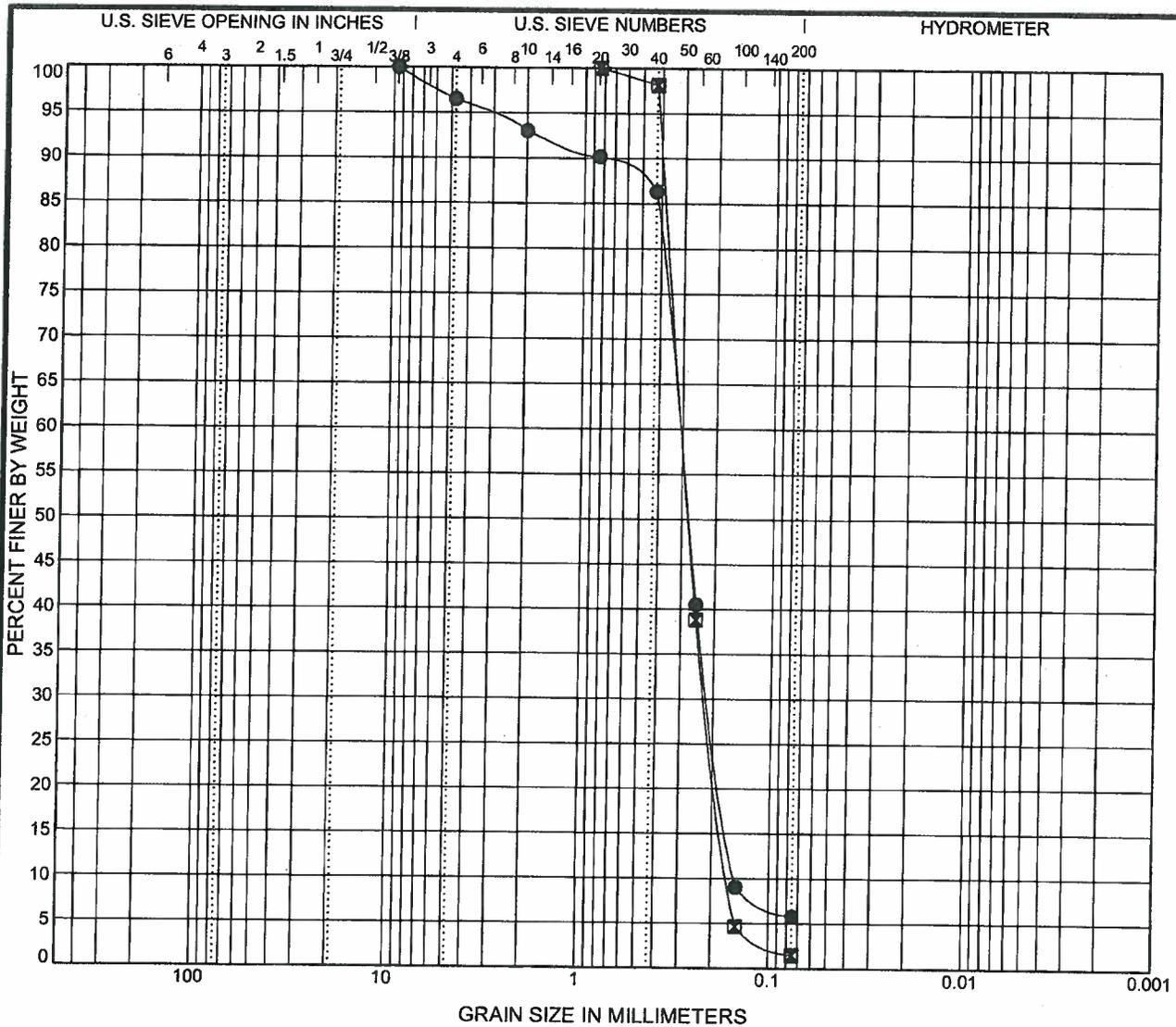
DUL\_BOREHOLE\_113-81079\_GOODWILL\_GINT.GPJ\_DUL\_GOLDER\_GDT\_11/14/11



DEPTH SCALE: 1 in to 3.8 ft  
 DRILLING CONTRACTOR: Engineering Partners Corporation  
 DRILLER: A. Senarighi

LOGGED: M. Krzewinski  
 CHECKED: A. Thorson  
 DATE: 11/11/2011

Figure  
3



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification	Depth (ft)	USCS Classification	LL	PL	PI	Cc	Cu
● G11-01 sample#2	2.0	SAND with silt and gravel (SP-SM)				0.9	2.1
☒ G11-01 sample#6	9.5	SAND (SP)				1.0	1.9

Specimen Identification	Depth (ft)	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
● G11-01 sample#2	2.0	9.5	0.31	0.21	0.15	3.5	90.7	5.7	
☒ G11-01 sample#6	9.5	0.8	0.3	0.22	0.16	0.0	98.6	1.4	



Golder Associates  
 4438 Haines Road  
 Duluth, MN 55811  
 Telephone: (218) 724-0088  
 Fax: (218) 724-0089

**Figure 4**  
**GRAIN SIZE DISTRIBUTION**

Project: Goodwill Industries - Loading Dock Addition  
 Number: 113-81079

US GRAIN SIZE 113-81079 GOODWILL GINT.GPJ DUL.GOLDER1-31-08.GDT 11/14/11